

**MOSFET/IGBT Drivers**  
Theory and Applications

## 1 Introduction

Modern Power Electronics makes generous use of MOSFETs and IGBTs in most applications, and, if the present trend is any indication, the future will see more and more applications making use of MOSFETs and IGBTs.

Although sufficient literature is available on characteristics of MOSFETs and IGBTs, practical aspects of driving them in specific circuit configurations at different power levels and at different frequencies require that design engineers pay attention to a number of aspects.

An attempt is made here to review this subject with some illustrative examples, and with a view to assist both experienced design engineers and those who are just initiated into this discipline.

### 1.1 MOSFET and IGBT Technology

Due to the absence of minority carrier transport, MOSFETs can be switched at much higher frequencies. The limit on this is imposed by two factors: transit time of electrons across the drift region and the time required to charge and discharge the input Gate and "Miller" capacitances.

IGBT derives its advantages from MOSFET and BJT topologies. It operates as a MOSFET with an injecting region on its Drain side to provide for conductivity modulation of the Drain drift region so that on-state losses are reduced, especially when compared to an equally rated high voltage MOSFET.

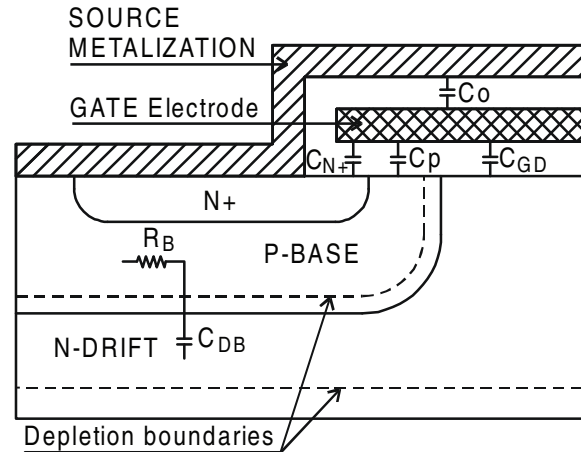
As far as driving the IGBT is concerned, it resembles a MOSFET and hence all turn-on and turn-off phenomena comments, diagrams, and Driver circuits designed for driving MOSFET apply equally well to an IGBT. Therefore, what follows deals only with MOSFET models.

### 1.2 MOSFET Models and Critical Parameters

**Figure 1** shows the internal cell structure of a DMOS MOSFET. As shown, the Gate to Source Capacitance consists of three components:  $C_P$ , the component created by the Gate Electrode over the P-base region;  $C_{N+}$ , created by the overlap of the Gate Electrode above the N+ source region; and  $C_O$ , arising due to the proximity of the Gate Electrode to the source metallization. In fact, all these are added to yield  $C_{GS}$ , which we call the Gate-to-Source Capacitance. It is this total value of capacitance that needs to be charged first

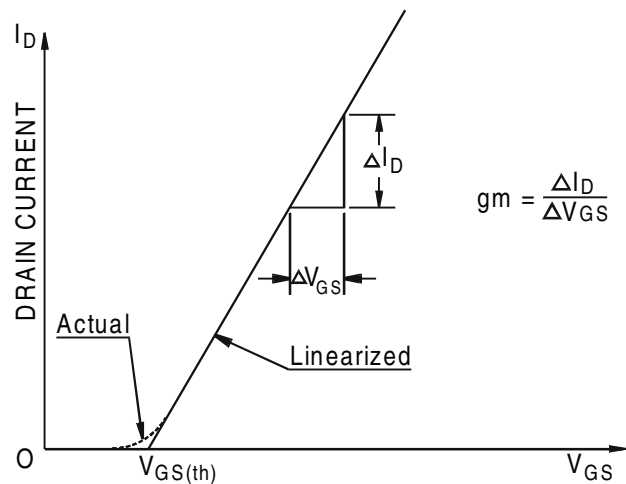
to a critical threshold voltage level  $V_{GS(th)}$ , before Drain Current can begin to flow.

**Figure 1 MOSFET Internal Structure**



The Gate-to-Drain capacitance,  $C_{GD}$  is the overlap capacitance between the Gate electrode and the N-drift Drain region.  $C_{GD}$  is sometimes referred to as the "Miller" capacitance, and contributes most to the switching speed limitation of the MOSFET. The junction capacitance between the drain to the P-Base region is  $C_{DS}$ . The P-Base region of the MOSFET is shorted to the N+ source. **Figure 2** shows a curve of  $I_D$  (Drain Current) versus  $V_{GS}$  (Gate Source Voltage). The graph has a slope ( $I_D / V_{GS}$ ) equal to  $g_m$ , which is called transconductance.

**Figure 2 Power MOSFET Transfer Characteristics**



Please note that the actual relationship between  $V_{GS}$  and  $I_D$  is shown by the dotted line and it can be

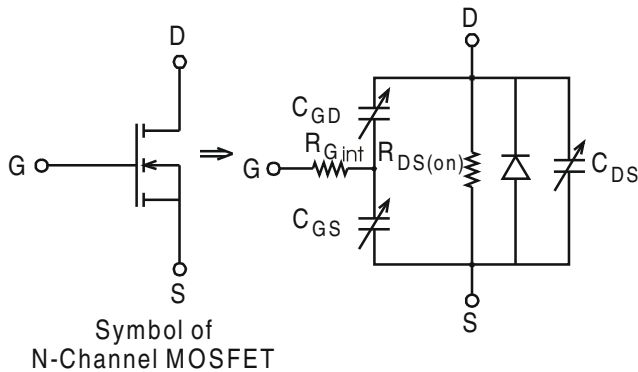
observed that in the vicinity of  $V_{GS(th)}$ , the relationship between  $V_{GS}$  and  $I_D$  is parabolic in nature:

$$I_D = K [V_{GS} - V_{GS(th)}]^2 \quad \text{Equation 1.1}$$

However, for Power MOSFETs, it is appropriate to consider the relationship to be linear for values of  $V_{GS}$  above  $V_{GS(th)}$ . The manufacturer's data sheet value of  $V_{GS(th)}$  is specified at 25°C.

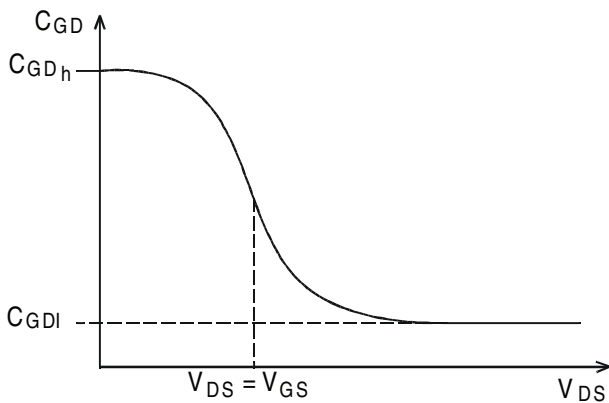
**Figure 3** shows a symbol of a N-Channel MOSFET and an equivalent model of the same with three inter-junction parasitic capacitances, namely:  $C_{GS}$ ,  $C_{GD}$ , and  $C_{DS}$ .

**Figure 3 MOSFET Symbol and Equivalent Circuit**



These are all shown as variable, as they indeed are. For example  $C_{GD}$  decreases rapidly as the Drain to Source voltage rises, as shown in **Figure 4**.

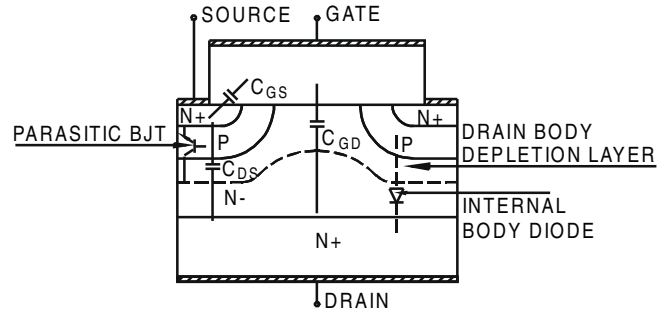
**Figure 4  $C_{GD}$  Variation With Respect to  $V_{DS}$**



In **Figure 4**, the high value of  $C_{GD}$  is called  $C_{GDh}$ , while the low value of  $C_{GD}$  is termed  $C_{GDI}$ .

**Figure 5** shows another cross-sectional view of a MOSFET with all these capacitances. In addition, It also shows the internal body diode and the parasitic BJT.

**Figure 5 N-Channel MOSFET Internal X-Section**

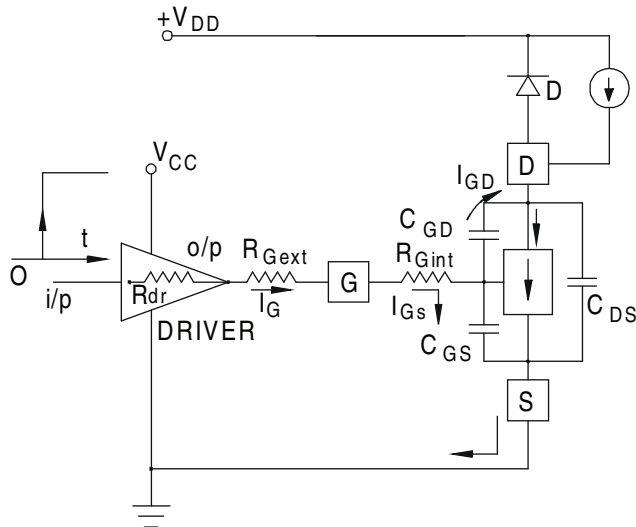


### 1.3 turn-on and turn-off Phenomena

#### 1.3.1 turn-on Phenomenon

To understand the turn-on and turn-off phenomena of the Power MOSFET, we will use a clamped inductive switching mode of operation, as it is the most commonly used.. This is shown in **Figure 6** and **Figure 7**. A model of the MOSFET is shown with all relevant components, which play a role in turn-on and turn-off events. As stated above, MOSFET's Gate to Source Capacitance  $C_{GS}$  needs to be charged to a critical voltage level to initiate conduction from Drain to Source. A few words of explanation will help understand **Figure 6** and **Figure 7**. The clamped inductive load is depicted by a current source with a diode, D, connected antiparallel across the inductor, and the MOSFET's intrinsic internal Gate resistance,  $R_{Gint}$ . As described above, the inter-junction parametric capacitances ( $C_{GS}$ ,  $C_{GD}$ , and  $C_{DS}$ ) are shown, and connected at their proper points.  $V_{DD}$  represents the DC Bus voltage applied to the Drain of the MOSFET through the clamped inductive load. The Driver is supplied by  $V_{CC}$  referenced by  $V_P$ , and its ground is connected to the common ground of  $V_{DD}$  and is returned to the Source of the MOSFET. The output from the Driver is connected to the Gate of the MOSFET through a resistor  $R_{Gext}$ .

**Figure 6 MOSFET Being Turned On by a Driver in a Clamped Inductive Load**



When a positive going pulse appears at the input terminal of the Driver, an amplified pulse appears at the output terminal of the Driver with an amplitude  $V_P$ . This is fed to the Gate of the MOSFET through  $R_{Gext}$ . As one can see, the rate of rise of voltage,  $V_{GS}$ , over the Gate and Source terminals of the MOSFET is governed by value of the total resistance in series ( $R_{dr} + R_{Gext} + R_{Gint}$ ) and total effective value of capacitance ( $C_{GS} + C_{GD}$ ).  $R_{dr}$  represents the output source impedance of the Driver.  $R_{Gext}$  is the resistance one generally puts in series with the Gate of a MOSFET to control the turn-on and turn-off speed of the MOSFET.

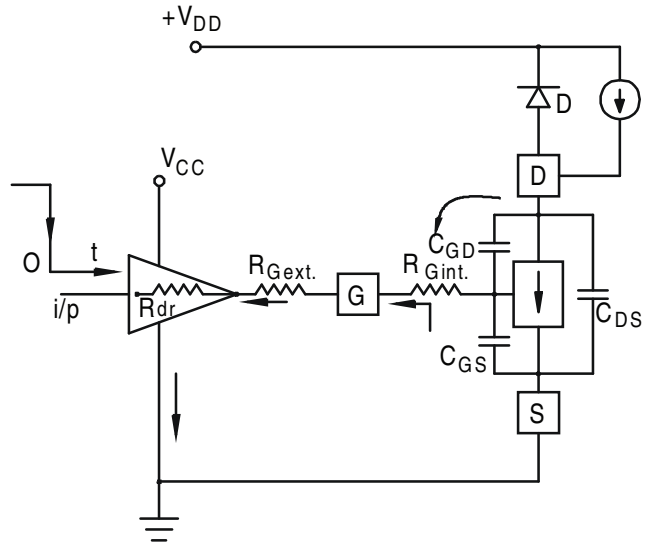
The waveforms shown in **Figure 8** depict the variation of these different parameters with respect to time, to help explain the entire turn-on sequence. In **Figure 6** and **Figure 7**, the free-wheeling diode, D, is assumed to be ideal with zero reverse recovery current. The waveforms shown in **Figure 8** are based on this assumption:

From time zero to  $t_1$ , ( $C_{GS} + C_{GD}$ ) is exponentially charged with a time constant:

$$T_1 = (R_{dr} + R_{Gext} + R_{Gint}) \times (C_{GS} + C_{GD})$$

until the gate-to-source voltage reaches  $V_{GS(th)}$ . In this time period, neither the drain voltage nor the drain current are affected, i.e. drain voltage remains at  $V_{DD}$  and the drain current is zero. This is also

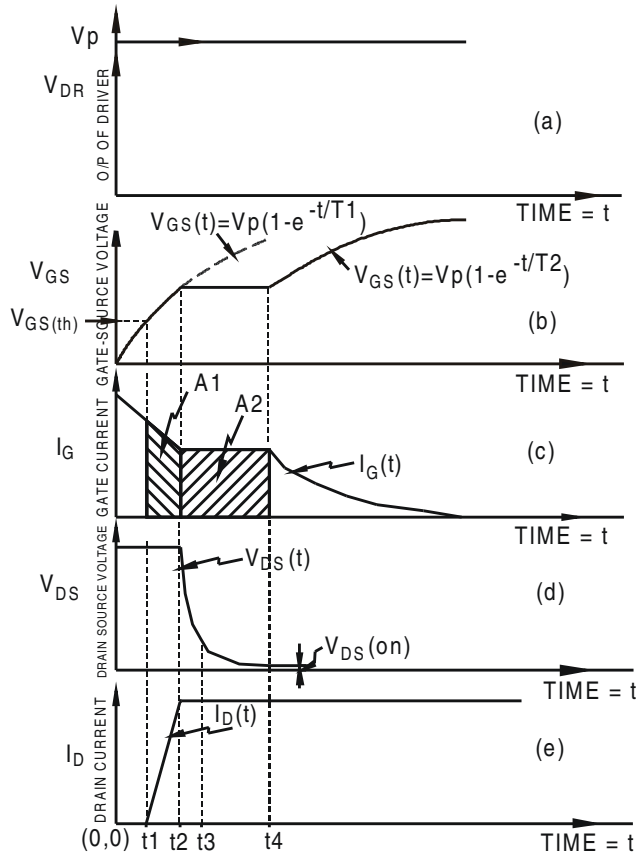
**Figure 7 MOSFET Being Turned Off by a Driver in a Clamped Inductive Load**



referred to as the turn-on delay. Note that between 0 to  $t_1$ , as  $V_{GS}$  rises,  $I_{GS}$  falls exponentially, since it essentially functions as an RC Circuit.

After time  $t_1$ , as the gate-to-source voltage rises above  $V_{GS(th)}$ , MOSFET enters a linear region as shown in **Figure 2**. At time  $t_1$ , drain current starts flowing, and the drain to source voltage  $V_{DS}$ , is still at  $V_{DD}$ . From the time  $t_1$  to  $t_2$ ,  $I_D$  increases rapidly and as shown in **Figure 4**,  $C_{GD}$  increases from  $C_{GDl}$  to  $C_{GDh}$  and the current available from the driver is diverted to charge this increased value of  $C_{GDh}$ . As outlined in **Figure 8**, between  $t_1$  and  $t_2$ , the drain current increases linearly with respect to  $V_{GS}$ . At time  $t_2$ , the gate to source voltage enters the Miller Plateau level and the drain voltage begins to fall rapidly, while the MOSFET is carrying full load current. During the time interval,  $t_2$  to  $t_4$ ,  $V_{GS}$  remains clamped to the same value as does  $I_{GS}$ . This is referred to as the Miller Plateau Region. During this interval, most of the drive current available from the driver is diverted to discharge the  $C_{GD}$  capacitance followed by a rapid drop of drain to source voltage. Only the external impedance in series with  $V_{DD}$  limits the drain current.

Figure 8 MOSFET turn-on Sequence



Beyond  $t_4$ ,  $V_{GS}$  begins to rise exponentially again with a time constant:

$$T_2 = (R_{dr} + R_{G_{ext}} + R_{G_{int}}) \times (C_{GS} + C_{GDh})$$

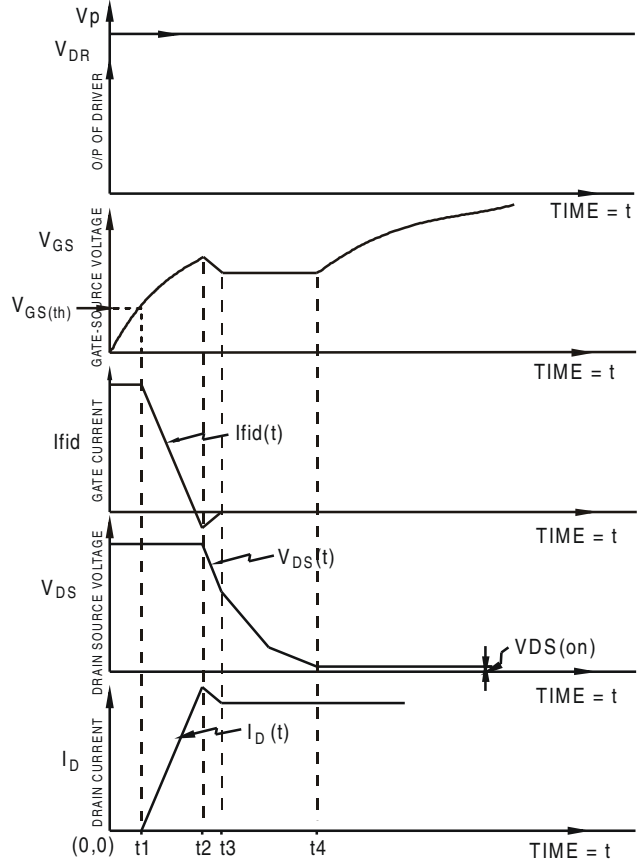
During this time interval the MOSFET approaches its final  $V_{GS}$  value effectively determining its  $R_{DS(on)}$ . At this point  $V_{DS}$  attains its lowest value as determined by:

$$V_{DS} = I_{DS} \times R_{DS(on)}$$

In **Figure 8**, A1 outlines the area of the  $I_G$  curve from time  $t_1$  to  $t_2$ . This represents the charge on  $(C_{GS} + C_{GD})$ , as it is the integration of the gate current  $I_G$  over a time period. Similarly, A2 represents the charge on  $C_{GD}$  from  $t_2$  to  $t_3$ , during which time the Miller effect is predominant.

If one considers the diode D not to be ideal, then the reverse recovery of the diode will influence the turn on behavior. Thus, the waveforms would look like what is depicted in **Figure 9**. As the diode undergoes reverse recovery, you can see a hump in the waveform of  $V_{GS}$  as well as  $I_D$  which occurs at approximately time  $t_2$ .

Figure 9 MOSFET turn-on Sequence Showing the Effect of Body Diode Reverse Recovery



### 1.3.2 turn-off Phenomenon

The turn-off phenomenon is shown in **Figure 10**. As can be expected, when the output from the driver drops to zero thereby turning off the MOSFET,  $V_{GS}$  initially decays exponentially from time 0 to  $t_1$  at the rate determined by time constant:

$$T_2 = (R_{dr} + R_{G_{ext}} + R_{G_{int}}) \times (C_{GS} + C_{GDh})$$

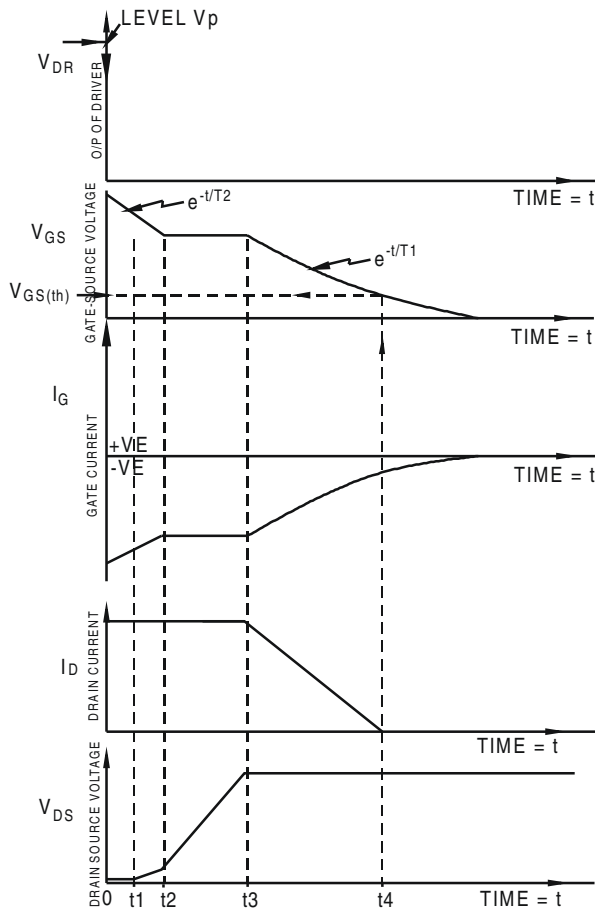
However, after  $t_4$ , it decays exponentially at the rate determined by:

$$T_1 = (R_{dr} + R_{G_{ext}} + R_{G_{int}}) \times (C_{GS} + C_{GDl})$$

Please note that the first delay in the turn off process is required to discharge the  $C_{ISS}$  capacitance from its initial value to the Miller Plateau level. From  $t = 0$  to  $t = t_1$ , the gate current is flowing through the  $C_{GS}$  and  $C_{GD}$  capacitances of the MOSFET. Notice that the drain current  $I_D$  remains unchanged during this time interval, but the drain source voltage,  $V_{DS}$ , just begins to rise. From  $t_1$  to  $t_2$ ,  $V_{DS}$  rises from  $I_D \times R_{DS(on)}$  towards its final off state value of  $V_{DS(off)}$ , where it is clamped to

the DC bus voltage level by the diode D. This time interval also corresponds to the Miller effect region as mentioned above in regards to the gate voltage, which results in a constant  $V_{GS}$ . During the time interval  $t_2$  to  $t_3$ , the  $V_{GS}$  begins to fall further below  $V_{GS(th)}$ .  $C_{GS}$  discharges through any external impedance between the gate and source terminals. The MOSFET is in its linear region and the drain current  $I_D$ , drops rapidly towards a zero value.  $V_{DS}$  was already at its off state value,  $V_{DS(off)}$  at the beginning of this interval therefore at  $t_4$ , the MOSFET is fully turned off.

Figure 10 MOSFET turn-off Sequence



The manufacturer’s Data Sheet for the MOSFET gives values of  $C_{ISS}$ ,  $C_{RSS}$ , and  $C_{OSS}$ . The following relationships help relate these to inter-junction parasitic capacitances described so far:

$$\begin{aligned}
 C_{GD} &= C_{RSS} \\
 C_{GS} &= C_{ISS} - C_{RSS} \\
 C_{DS} &= C_{OSS} - C_{RSS}
 \end{aligned}
 \tag{Equation 1.2}$$

As  $C_{GD}$  and  $C_{DS}$  capacitances are dependent on  $V_{DS}$ , the data sheet values are valid only at specified test conditions. Equation 1.3 can be used to calculate the average effective values of these capacitances.

Equation 1.3

$$\begin{aligned}
 \text{Effective } C_{GD} &= 2(C_{RSS \text{ specified}})(V_{DS, \text{specified}}/V_{DS, \text{off}})^{1/2} \\
 \text{Effective } C_{OSS} &= 2(C_{OSS \text{ specified}})(V_{DS, \text{specified}}/V_{DS, \text{off}})^{1/2}
 \end{aligned}$$

### 1.4 Power Losses In Drivers And Driven MOSFET / IGBT

To determine the power loss in a Driver while driving a power MOSFET, refer to equation 1.4 and the gate charge  $Q_G$  vs.  $V_{GS}$  curve for different values of  $V_{DS(off)}$  found in the MOSFET’s data sheet.

Equation 1.4

$$P_{GATE} = V_{CC} \times Q_G \times f_{sw}$$

$V_{CC}$  is the Driver’s supply voltage,  $Q_G$  is the total gate charge of the MOSFET being driven, and  $f_{sw}$  is the switching frequency. Clearly then, it is prudent then to choose a MOSFET with lower value of  $Q_G$ .

As shown in **Figure 8**, **Figure 9**, and **Figure 10** in regards to MOSFET switching losses, there are some short time-intervals during which a finite  $V_{DS}$  and  $I_D$  co-exist. When this happens during turn-on, the actual integration:

Equation 1.5

$$\int V_{DS}(t)I_D(t)dt$$

is defined as turn-on switching energy loss. Likewise, during turn-off, when finite values of  $I_D$  and  $V_{DS}$  coexist, the integration of:

Equation 1.6

$$\int V_{DS}(t)I_D(t)dt$$

is called turn-off switching energy loss in a MOSFET. Amongst the responsible parameters in determining these switching energy losses,  $C_{ISS}$ ,  $C_{OSS}$ , and  $C_{RSS}$  affect the turn-on and turn-off delays as well as the turn-on and turn-off times.

For an IGBT, it would be similarly shown that:

Equation 1.7

$$\int V_{CE}(t)I_C(t)dt$$

represents the switching energy loss. The time interval for these integrals would be the appropriate time during which finite values of  $I_D$  and  $V_{DS}$  or  $V_{CE}$  and  $I_C$  coexist

in a MOSFET or IGBT respectively. Average switching energy lost in the device can be computed as follows:

$$\text{MOSFET: } P_s = 1/2 \cdot V_{DS} \cdot I_D \cdot f_{sw} \cdot (t_{on} + t_{off})$$

Equation 1.8

$$\text{IGBT: } P_s = 1/2 \cdot V_{CE} \cdot I_C \cdot f_{sw} \cdot (t_{on} + t_{off})$$

Equation 1.9

The main emphasis in modern Power Electronics is to reduce the total losses dissipated in devices and subsystems, strive for higher operating efficiency and achieving more compact designs, thereby reducing volume and weight of resultant systems. Since operation at higher and higher switching frequencies is now a necessity, and, as a result, switching losses predominate in the power-loss-budget in semiconductor switches. Reducing switching losses then becomes the single most crucial goal. Keeping this goal in mind, the entire line of IXYS MOSFET/IGBT Drivers are designed to facilitate the design of drive circuits that yield fast rise and fall times.



## 2 Types of Drivers

### 2.1 IC Drivers

Although there are many ways to drive MOSFETs and IGBTs using hard wired electronic circuits, IC Drivers offer convenience and features that attract designers. The foremost advantage is compactness. IC Drivers intrinsically offer lower propagation delay. As all important parameters are specified in an IC Driver, designers need not go through the time-consuming process of defining, designing, and testing circuits to drive MOSFET/IGBTs.

### 2.2 Techniques Available to Boost Current Outputs

A totem-pole stage, with N-Channel and P-Channel MOSFETs, can be used to boost the output from an IC Driver. The disadvantage is that the signal is inverted, and a “shoot-through” condition may exist when the common gate voltage is in transition.

A totem-pole arrangement using matched NPN-PNP transistors, on the other hand, offers many advantages, while boosting the output currents from IC Drivers. The shoot-through phenomenon is absent in this case. The pair of transistors protects each other’s base-emitter junctions and handles current surges quite well. One such arrangement is shown in **Figure 17**. Here Q1 is a NPN transistor, while Q2 is a matched PNP transistor with appropriate collector current rating and switching speed to satisfy the drive requirement for the high-power IGBT. Another feature added is a negative  $V_e$  bias ( $-V_e$ ) for guaranteed fast switch turn-off even in an electrically noisy environment. This is done by utilizing a power supply with +15 and –5 Volts outputs, whose common ground is connected to the IGBT emitter.

IXDD609 is a very high speed IC Driver with extremely short rise and fall times and propagation delays. Its  $V_{CC}$  rating is  $35V_{DC}$  and can actually deliver 9A peak output current. The arrangement shown in **Figure 17** does a few more things in addition to boosting the output current still higher. It allows one to choose different turn-on and turn-off times by selecting different values of  $R_{Gon}$  and  $R_{Goff}$ . It allows for incorporating  $-V_e$  bias for reasons explained above. A pair of 18V Zener diodes with their cathodes connected together protects the gate-emitter junction of the IGBT from voltage spikes.

### 2.3 Techniques To Generate $-V_e$ Bias During turn-off

The importance of  $-V_e$  bias during turn-off for practically all semiconductor switches cannot be overemphasized, as one may recall from the days of Bipolar transistors. This helps to quickly remove any charge on the  $C_{GS}$  and  $C_{GD}$  in the case of MOSFETs and IGBTs, thus considerably accelerating turn-off.

It is important to understand that turn-on speed of a MOSFET or IGBT can be increased only up to a level matched by the reverse recovery of rectifiers or diodes in a power supply, because in an inductive clamped load (most common), the turn-on of a MOSFET or IGBT coincides with the turn-off (or reverse recovery completion) of the rectifier diode. Any turn-on faster than this does not help. Too fast a turn-on could also cause oscillation in the drain or collector current. However, it is always beneficial to have a driver with an intrinsic low turn-on time, and then being able to tailor this with a series gate resistor.

The turn-off phenomenon, on the other hand, does not have to wait for any other component in the subsystem. It is here that any enhancement technique can be utilized. Although IXYS drivers by themselves feature extremely low turn-on and turn-off times, an arrangement to provide  $-V_e$  bias during turn-off helps provide for a faster turn-off, and also prevents a false turn on even in an electrically noisy environment.

**Figure 21** shows how to generate  $-V_e$  bias in a transformer coupled drive circuit arrangement. Here a Zener diode can be chosen of appropriate voltage for giving that much  $-V_e$  bias (plus one diode drop) during turn-off. Another unique feature of the circuit in **Figure 21** is its ability to maintain an exact pulse waveform across the gate and source. As shown in **Figure 19**, an isolated DC to DC converter with outputs of +15V and –5V is used to power the IXDD614. When the isolated ground of this DC to DC Converter is connected to the emitter of the IGBT being driven, –5V of  $-V_e$  bias voltage during provides for a faster turn-off time.

### 2.4 Need for Under-Voltage Protection

**Figure 2** shows depicts a typical transfer characteristics ( $I_D$  vs.  $V_{GS}$ ) of a MOSFET. As can be seen for values of  $V_{GS}$  below  $V_{GS(th)}$  the drain current is negligible, but in this vicinity, the device is in its linear (Ohmic) region and concurrent application of large



values of  $V_{DS}$  could cause a considerable amount of localized heating of the junction. In short, when a MOSFET is being used as a switch, any operation in its linear region could cause overheating or device failure. Bringing the MOSFET quickly into saturation from its off-state is the driver's function. If  $V_{CC}$  falls below the minimum required value, linear operation can ensue to the disadvantage of the MOSFET. Note, however that most PWM ICs, controller ICs and microcomputer ICs have this protection feature built-in, and, if sharing the same  $V_{CC}$  bus, the driver IC gets the benefit of this function being implemented elsewhere in the subsystem.

## 2.5 Overload / Short Circuit Protection

Any operation of the MOSFET/IGBT outside the Safe Operating Area (SOA) could cause overheating and eventual device failure, and should be prevented by an electronic active monitoring and corrective arrangement.

Load or current sensing could be done by either a Hall Effect Sensor or by a Shunt resistor in series with source/ emitter terminal. The voltage picked up, which is proportional to current, is low pass filtered and then compared to a preset limit. The comparator output could initiate turn-off of MOSFET/IGBT. A circuit to detect an overload/short circuit is shown in **Figure 19**, where the output FAULT will go low when it occurs.

All IXDD-series drivers have an ENABLE pin, which, when driven low, say, by the FAULT output from this comparator, puts the final N-channel and P-channel MOSFETs of the IXDD Driver in their TRISTATE mode. This not only stops any output from the driver, but also provides an environment for implementing a "soft turn-off". To accomplish this, a resistor of sufficient value is connected from the gate to the source/emitter of the MOSFET. As a result, the  $C_{GS}$  gets discharged through this resistor and, depending on the value of the connected resistor, a soft turn-off of any duration can be achieved. Another way, as shown in **Figure 12**, is to use a signal MOSFET, Q1, to pull down the gate when a short circuit is detected. The resistor in series with this signal MOSFET determines the time duration of this soft turn-off. Soft turn-off helps protect the IGBT/ MOSFET from any voltage transients generated due to  $LdI_C/dt$  (or  $LdI_D/dt$ ) that could otherwise bring about avalanche breakdown. The PC board layout for this circuit is shown in **Figure 13**.

For an IGBT, de-sat detection (de-sat = desaturation of forward voltage drop) is a method used for short circuit/

overload protection. When a short circuit/overload occurs, the forward voltage drop of the IGBT ( $V_{CE}$ ) rises to disproportionately high values. One must ignore the initial turn-on rise in  $V_{CE}$ , when output from the driver has still not risen to a high enough value. Nevertheless, when  $V_{CE}$  rises to a level of, say, 7 Volts, in presence of sufficient gate drive voltage, it means the collector current  $I_C$  has risen to a disproportionately high value, signaling overload. When a voltage level higher than 6.5V is detected, resulting in soft turn-off of the IGBT. **Figure 19** shows how the de-sat feature can be wired into a total driver circuit, using also other features, such as opto-isolation and -Ve turn-off bias.

### 3 High Side Driving Techniques

#### 3.1 Employing Charge-Pump and Bootstrap Methods

The Bootstrap Technique as shown in **Figure 15**. The basic bootstrap building elements are the level shift circuit; bootstrap diode, DB; level shift transistor, Q1; bootstrap capacitor, CB; and IXDD609 or IXDD614. The bootstrap capacitor, IXDD609/IXDD614 driver, and the gate resistor are the floating, source-referenced parts of the bootstrap arrangement. The disadvantages of this technique are longer turn-on and turn-off delays, and 100% duty cycle is not possible. Also, the driver has to overcome the load impedance and negative voltage at the source of the device during turn-off.

#### 3.2 Achieving Galvanic Isolation By Using Optocouplers To Drive Upper MOSFET/IGBT

For driving high-side MOSFET/IGBT in any topology, optocouplers can be used with the following advantages:

- Optocouplers provide a very high isolation voltage: 2500V to 5000V of isolation is achievable with careful selection.
- Optocouplers can handle signals from DC to several MHz.
- Optocouplers are easily interfaced to controller ICs, micro-computers, or any PWM IC.

One disadvantage is that the optocoupler adds its own propagation delay. Another disadvantage is that a separate, isolated power supply is required to feed the output side of the optocoupler and the driver connected to it. However, isolated DC to DC Converters with a few thousand Volts of isolation are readily available. These can be used to supply isolated and regulated +Ve 15V and -Ve 5V to the output side of the optocoupler and the driver IC for driving upper MOSFET/IGBT as is shown in **Figure 19** and **Figure 20**. As can be seen, an identical chain of optocouplers, drivers, and DC to DC converters are used for even lower IGBTs. This is done to guarantee identical propagation delays for all incoming IGBT gate signals.

#### 3.3 Use Of Transformers To Obtain Galvanic Isolation in Driving Upper MOSFET/IGBT

Using transformers to achieve galvanic isolation is a very old technique. Depending on the range of frequencies being handled and power rating (voltage and current ratings and ratios), transformers can be

designed to be quite efficient. The gate drive transformer carries very small average power, but delivers high peak currents at turn-on and turn-off of the MOSFET/IGBT.

While designing or choosing a gate drive transformer, keep the following points in mind:

- The average power of the transformer can accept should be used as a design guideline. A margin of safety should be taken into account, keeping in mind the maximum volt-second product and allowing for worst case transients with maximum duty ratio and maximum input voltage possible.
- Employing bifilar winding techniques to eliminate any net DC current in any winding. This is to avoid core saturation.
- If operation in any one quadrant of B-H loop is chosen, care should be taken for resetting the core.

Advantages of employing transformers for Gate Drive are:

- There is no need for any isolated DC to DC Converter for driving an upper MOSFET/IGBT .
- There is practically no propagation delay time in a transformer to carry signals from primary side to the secondary side.
- Several thousand volts of isolation can be built-in between windings by proper design and layouts.

The disadvantages of using transformers for Gate Drive are:

- They can be used only for AC signals.
- Large duty ratios cannot be handled by the transformer without being saturated by net DC, unless AC coupling capacitors are employed in series.

Two examples of gate Drive circuits, using transformers follow. In **Figure 18**, a phase shift controller outputs its signals to the IXDD604 dual drivers, which in turn, feed the transformers. The secondary windings of these transformers are coupled to the Gates of upper and lower MOSFETs in an "H" Bridge topology. **Figure 21** shows another transformer coupled gate drive circuit employing a DC restore technique to maintain the same waveshape as the original signal with the added feature of -Ve bias offered using a Zener in series with a fast diode across the secondary.

## 4 IXYS Line of MOSFET and IGBT Drivers

IXYS offers the following MOSFET/IGBT drivers:

- IXD\_602: Dual 2A, Ultrafast Driver
- IXD\_604: Dual 4A, Ultrafast Driver, w/Enable
- IXD\_609: 9A, Ultrafast Driver, w/Enable
- IXD\_614: 14A, Ultrafast Driver, w/Enable
- IXD\_630: 30A, Ultrafast Driver, w/Enable

### 4.1 General Remarks About IXD\_600 Series Of Drivers

The most important strength of these drivers is their ability to provide the high currents needed to adequately drive today's and tomorrow's large size MOSFETs and IGBTs. This is made possible by devoting a large portion of the silicon die area to creating a high current (NMOS and PMOS) output stage. Another important feature of these drivers is that there is no cross conduction, thus giving almost 33% lower transition power dissipation.

In addition, some of these Drivers incorporate a unique facility to disable the output by using an ENABLE pin. When this pin is driven LOW in response to detecting an abnormal load current, the driver output enters its tristate (high impedance state) mode, and a soft turn-off of the MOSFET/IGBT can be achieved. This helps prevent damage that could occur to the MOSFET/IGBT due to a  $dI/dt$  overvoltage transient, if it were to be switched off abruptly, "L" representing the total inductance in series with Drain or Collector. A suggested circuit to accomplish this soft turn off upon detecting overload or short circuit is shown in **Figure 12**. It is also possible to do this by an independent short circuit/overload detect circuit, which could be a part of the PWM or other controller IC. All one needs to do is to take an output signal (FAULT) from such a circuit, and feed it into the ENABLE pin of the driver. A resistor,  $R_P$ , connected across gate and source or gate and emitter (as the case may be) would ensure soft turn-off of the MOSFET/IGBT, turn-off time being equal to  $R_P(C_{GS} + C_{GD})$

Detailed specifications of these IXD\_600 series of drivers are available on IXYS's web site:

<http://www.ixysic.com/Products/IGBT-MOSFETDvr.htm>

#### 4.1.1 IXD\_604

IXD\_604 is a dual 4A driver, which is useful in many circuits employing two MOSFETs or IGBTs. It could also be used for two MOSFETs/IGBTs connected in a phase leg configuration. While using high voltage DC

supplies for driving the phase leg, H-Bridge, or 3-phase bridge circuits, some technique for achieving galvanic isolation of the upper MOSFET/IGBT drivers is required, in addition to making a provision for the isolated power supplies.

**Figure 18** shows an interesting application for IXDD604 in a phase shift PWM controller application, in which galvanic isolation is obtained by using ferrite core gate drive transformers. Note that this controller operates at a fixed frequency. Turnoff enhancement is achieved by using local PNP transistors.

IXDD604 provides a simple answer for driving a vast number of low and medium current MOSFETs and IGBTs.

#### 4.1.2 IXD\_609 AND IXD\_614

The IXD\_609 is eminently suitable for driving higher current MOSFETs and IGBTs, however the IXD\_614 can drive larger size MOSFET/IGBT Modules. Many circuit schematics applying these in various topologies are possible, and some of these are shown at the end of this application note.

The 5-pin TO-263 surface mount version can be soldered directly on to a copper pad on the printed circuit board for better heat dissipation. It is possible then to use these high current drivers for very high frequency switching application, driving high current MOSFET modules for a high power converter/inverter.

**Figure 11** shows a basic low side driver configuration using the IXDD609 or IXDD614.  $C_1$  is used as a bypass capacitor placed very close to pins #1 and #8 of the driver IC. **Figure 16** shows a method to separately control the turn-on and turn-off times of the MOSFET/IGBT. turn-on time can be adjusted by  $R_{G_{on}}$ , while the turn-off time can be varied by  $R_{G_{off}}$ . The diodes in series are fast diodes with a low forward voltage drop. The 18V, 400mW Zener diodes protect the gate-emitter junction of the IGBT. When laying out a PCB, the trace length between pins #6 and #7, and the IGBT gate pins should be as short as possible. Also, providing a generous copper surface for a ground plane helps achieve fast turn-on and turn-off times without creating oscillation in the drain/collector current.

**Figure 16** also shows another arrangement, and includes a method for faster turn-off using a PNP transistor placed very close to the MOSFET gate and source. It is a good practice to tie the ENABLE pin of

drivers to  $V_{CC}$  through a 10k $\Omega$  resistor. This ensures that the driver always remains in its ENABLED mode, except when driven low due to a FAULT signal. Again, this FAULT signal puts these two drivers into their TRISTATE output mode.

**Figure 17** shows a method to boost output from IXDD609 to a much higher level for driving a very high power IGBT module. Here the turn-on and turn-off times can be varied by choosing different values of resistors,  $R_{g_{on}}$  and  $R_{g_{off}}$ . To provide a -Ve bias of 5V, the IGBT emitter is grounded to the common of +15V and -5V power supplies, which feeds +15V and -5V to the IXDD609. Notice that the incoming signals must also be level shifted.

**Figure 19** shows an IXDD614 driving one IGBT of a Converter Brake Inverter (CBI) module. Here all protection features are incorporated. For high temperature cutoff, a bridge circuit is used with the CBI module's thermistor. Comparator U3 compares the voltage drop across the thermistor to the stable voltage from the Zener diode. P1 can be used to preset the cutoff point at which the comparator's output goes low. This is fed into the microcomputer as an OVERTEMP signal.

Short circuit protection is provided by continuously monitoring the voltage drop across a SHUNT. Note that one end of SHUNT is connected to the power supply ground GND1. The voltage picked up from this SHUNT is amplified by a low noise op-amp, and is then compared to the stable voltage from the same Zener. When a short circuit occurs, the comparator output (FAULT) goes low. 1% metal film resistors are used throughout in both these circuits to ensure precision and stability. C3 and C4 help in offering low-pass filtering to avoid nuisance tripping.

Principle of DESAT sensing for detecting overload on an IGBT has been explained before, [see "Overload / Short Circuit Protection" on page 9](#). In the case of an AC Motor Drive, each IGBT has to be protected from overload using separate DESAT sensing. **Figure 19** and **Figure 20** show the connection for each IGBT. DESAT sensing is done on the isolated side of each optocoupler, while the resultant FAULT signal is generated on the common input side with respect to GND1. Each FAULT signal is open-collector type and hence can be tied together with other FAULT signals from other optocoupler or from other comparators. The microcomputer will stop output drive signals when either the FAULT or the OVERTEMP signal goes low.

When this happens, notice that IXDD614 offers a -Ve bias of -5V to guarantee turn-off conditions, even in the presence of electrical noise. -5V is applied to the gate of each IGBT during turn-off even under normal operating conditions. After the fault is cleared, the microcomputer can issue a RESET signal for resuming normal operation.

## 5 Practical Considerations

When designing and building driver circuits for MOSFETs and IGBTs, several practical aspects have to be taken into consideration to avoid prevent voltage spikes, oscillation or ringing, and false turn-on. More often than not, these are a result of improper or inadequate power supply by-passing, layout and mismatch of driver to the driven MOSFET/IGBT.

As we now understand, turning a MOSFET or an IGBT on and off amounts to charging and discharging large capacitive loads. Suppose we are trying to charge a capacitive load of 10,000 pF from 0V<sub>DC</sub> to 15V<sub>DC</sub> (assuming we are turning on a MOSFET) in 25 ns, using the IXDD614, which is a 14A, ultra high speed driver.

Equation 5.1

$$I = \Delta V \times C / \Delta t$$

$$I = [(15-0) \times 10000 \times 10^{-12} / 25 \times 10^{-9}] = 6A$$

$$I = 6A$$

What this equation tells us is that current output from the driver is directly proportional to the voltage swing and/or the load capacitance, and inversely proportional to rise time. Actually the charging current would not be steady, but would peak around 9.6A, well within the capability of IXDD614. However, IXDD614 will have to draw this current from its power supply in just 25 ns. The best way to guarantee this is by putting a pair of by-pass capacitors (of at least 10 times the load capacitance) of complementary impedance characteristics in parallel, very close to the V<sub>CC</sub> pin of IXDD614. These capacitors should have the lowest possible ESR (Equivalent Series Resistance) and ESL (Equivalent Series Inductance). One must keep the capacitor lead lengths to the bare minimum.

Another very crucial point is proper grounding. Drivers need a very low impedance path for current return to ground, to avoid ground loops. The three paths for returning current to ground are:

- Between IXDD614 and the logic driving it.
- Between IXDD614 and its own power supply.
- Between IXDD614 and the source/emitter of the MOSFET/IGBT being driven.

All these paths should be extremely short in length to reduce inductance and be as wide as possible to reduce resistance. Also, these ground paths should be kept distinctly separate to avoid returning ground current from the load to affect the logic line driving the IXDD614. A good method is to dedicate one copper plane in a multilayered PCB to provide a ground

surface. All ground points in the circuit should return to the same physical point to avoid generating differential ground potentials.

With desired rise and fall times in the range of 25 to 50ns, extreme care is required to keep lengths of current carrying conductors to the bare minimum. Since every inch of length adds approximately 20 nH of inductance, a di/dt of 240 Amps/microsecond (used in the example calculation for Equation 5.1) generates a transient Ldi/dt voltage of 4.8V per inch of wire length, which subtracts from the driver's output. The real effect will be a significant increase in rise time for every tiny increase in conductor length from the output pin of the driver to the gate lead of the MOSFET/IGBT. For example, one extra inch of conductor length could increase rise time from 20ns to 70ns in an ultra high speed gate drive circuit. Another detrimental effect of longer conductor length is transmission line effect and resultant RFI/EMI.

It is prudent to also keep in mind the fact that every MOSFET/IGBT has some inductance depending on the package style and design. The lower this value, the better is the switching performance, as this inductance is, in effect, in series with the source/emitter, and the resulting negative feedback increases switching times. IXYS MOSFETs and IGBTs are housed in packages that have extremely low intrinsic inductance.

When using a driver IC for any application, it is also necessary to compute the power dissipated in the driver for a worst-case scenario. The total power dissipated in the driver IC is the sum of the following:

- Capacitive load power dissipation;
- Transition power dissipation;
- Quiescent power dissipation.

For all members of the IXD\_609 series of drivers, transition power dissipation is absent due to a unique method (patent pending) of driving the output N-channel and P-channel MOSFETs that practically eliminates cross conduction.

As described earlier, [see “Power Losses In Drivers And Driven MOSFET / IGBT” on page 6](#), a MOSFET/IGBT driver incurs losses. The formula to calculate the power loss in a driver is:

Equation 5.2

$$P_{D(on)} = \frac{D \times R_{OH} \times V_{CC} \times Q_g \times f_{sw}}{R_{OH} + R_{Gext} + R_{Gint}}$$



$$P_{D(off)} = \frac{(1-D) \times (R_{OL} \times V_{CC} \times Qg \times fsw)}{R_{OL} + R_{Gext} + R_{Gint}} \quad \text{Equation 5.3}$$

where:

- $R_{OH}$  = Output resistance of driver @ output High
- $R_{OL}$  = Output resistance of driver @ output Low
- $fsw$  = Switching frequency
- $R_{Gext}$  = resistance kept externally in series with gate of MOSFET/IGBT
- $R_{Gint}$  = Internal mesh resistance of MOSFET/IGBT
- $D$  = Duty Cycle (Value between 0.0 to 1.0)
- $Qg$  = Gate Charge of MOSFET/IGBT

$$\text{Total loss } P_D = P_{D(on)} + P_{D(off)}$$

Note also that, in general,  $R_{Gint}$  is small and can be neglected, and that  $R_{OH} = R_{OL}$  for all IXD\_600 series drivers. Consequently, if the external turn-on and turn-off gate resistors are identical, then the total driver power dissipation formula simplifies to:

$$P_D = P_{D(on)} + P_{D(off)} = \frac{R_{OH} \times V_{CC} \times Qg \times fsw}{R_{OL} + R_{Gext}} \quad \text{Equation 5.4}$$

As an example:

- Assume that we are driving an IXFN200N10P for a telecom power supply application or for a UPS/ Inverter application at a switching frequency of 20 kHz.
- $R_{Gext} = 4.7$  Ohms and gate supply voltage is 10V.

In the IXDD609 Data sheet, we read the value of  $R_{OH}=2\Omega(\text{max})$  and  $R_{OL}=1.5\Omega(\text{max})$ . For  $Qg$ , refer to the data sheet for the IXFN200N10P from [www.ixys.com](http://www.ixys.com), and go to its Gate Charge vs.  $V_{GS}$  curve. Look for the value of  $Qg$  at  $V_{GS}=10V$ . You can read it as approximately 235nC. Substituting these values into Equation 5.4 yields:

$$P_D = \frac{2 \times 15 \times 235 \times 10^{-9} \times 20000}{1.5 + 4.7}$$

$$P_D = 22.74\text{mW}$$

Assuming an ambient temperature of 50°C in the vicinity of the IXDD609PI, the power dissipation capability of IXDD609PI must be derated by 8mW/°C, which is 200mW. The maximum allowable power dissipation at this temperature becomes 1000-200=800mW. However, as calculated above, we will be dissipating only 22.74mW, so we are well within the dissipation limit of 777.26mW.

If one increases  $fsw$  to 500kHz for a DC to DC converter application, keeping other parameters the same as above, now the dissipation would be 569mW. Again we are still within the dissipation limit of 231mW.

Another example: A boost converter, using IXFK55N50 at  $V_{DS}=250V_{DC}$  and at  $I_D=27.5A$ . Assume that  $fsw=500\text{kHz}$  and  $V_{CC}=12$  V. From the curve of Gate Charge for the IXFK55N50 in its data sheet, one can determine that  $Qg=370\text{nC}$ . Set  $R_{Gext}=1\Omega$ . We use IXDD614YI or IXDD614CI here, both of which can dissipate 12W. Here, the maximum value of  $R_{OH}=1.5\Omega$ ,  $R_{OL}=1.2\Omega$ . Substituting the above values in the equation, the power dissipation is computed to be:

$$P_D = \frac{1.5 \times 12 \times 370 \times 10^{-9} \times 500000}{1.2 + 1}$$

$$P_D = 1.51\text{W}$$

For the third example, consider driving the large size MOSFET module, VMO 580-02F with IXD\_630YI, at  $fsw=250\text{kHz}$ . Let  $V_{CC}=10V$ ,  $R_{OH}=0.17\Omega$ ,  $R_{OL}=0.16\Omega$ ,  $R_{Gext}=0\Omega$ . From the data sheet:  $Qg=2750\text{nC}$  at  $V_{CC}=10$  V. Substituting:

$$P_D = \frac{0.17 \times 10 \times 2750 \times 10^{-9} \times 250000}{0.16 + 0}$$

$$P_D = 7.3\text{W}$$

IXDD630YI (TO-263) or IXDD630CI (TO-220) can easily drive this load provided adequate heatsinking and proper air flow are maintained. Comments above for mounting TO-263 and TO-220 packages apply here as well. For derating use 0.1W/°C. So for an ambient temperature of 50°C, the answer is 2.5 W. As the limit of IXDD630YI or IXDD630CI is 12 W, subtracting 2.5W from this yields 9.5W; therefore, 7.3W is possible with or without a proper heat sink. Thermal impedance (junction to case) is 0.55°C/W for TO-263 and TO-220, hence a rise in case temperature should be within limit. If we increase  $V_{CC}$  to 15V, then conduction losses in the MOSFET could reduce due to lower  $R_{DS(on)}$ , but obtaining the same rise and fall times will incur more power loss in the driver due to increased  $V_{CC}$  and  $Qg$ . If that happens, the approach described in **Figure 17** can be employed.

## 6 Conclusion

With proliferating applications of modern power electronics worldwide, faster, more efficient and more compact MOSFETs and IGBTs are replacing older solid state and mechanical devices. The design of newer and more efficient techniques to turn these solid state devices on and off is a subject that requires thorough study and understanding of the internal structure and dynamic processes involved in the working of MOSFET/IGBTs.

With the advent of IC drivers for these fast MOSFET/IGBTs, the designer is relieved of the tedious task of designing elaborate driver circuits. Nevertheless, understanding these newer ICs, their strengths and limitations, is of paramount importance. Different configurations for particular topologies call for specific application knowledge. Illustrations are the best way to explain theory and applications of these IC drivers. Practical use of these IC drivers calls for great care for achieving near theoretical results.



## 7 References:

1. B. Jayant Baliga, "Power Semiconductor Devices", PWS Publishing Company, Boston, MA (1996)
2. Ned Mohan, Tore M. Undeland, William P. Robbins: "POWER ELECTRONICS: Converters, Applications and Design", John Wiley & Sons, New York (1994)
3. Power Supply Design Seminar - 2001 series, Unitrode Products from Texas Instruments.

Figure 11 Using IXDD609 or IXDD614 to Drive an IGBT

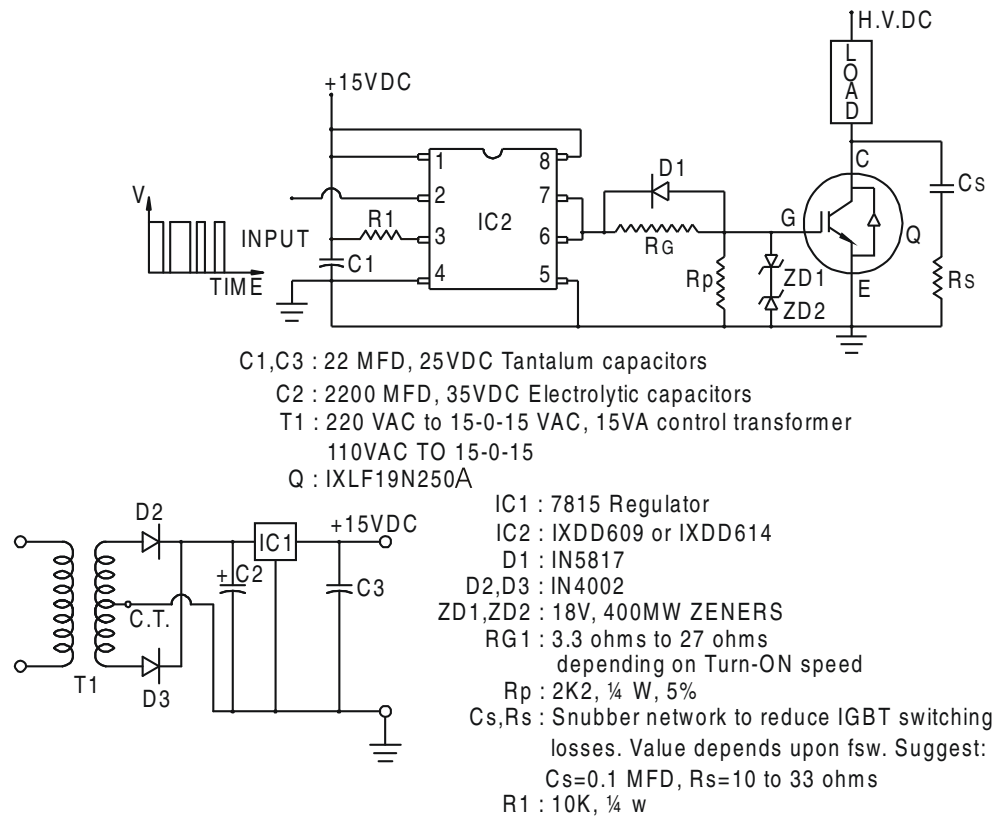
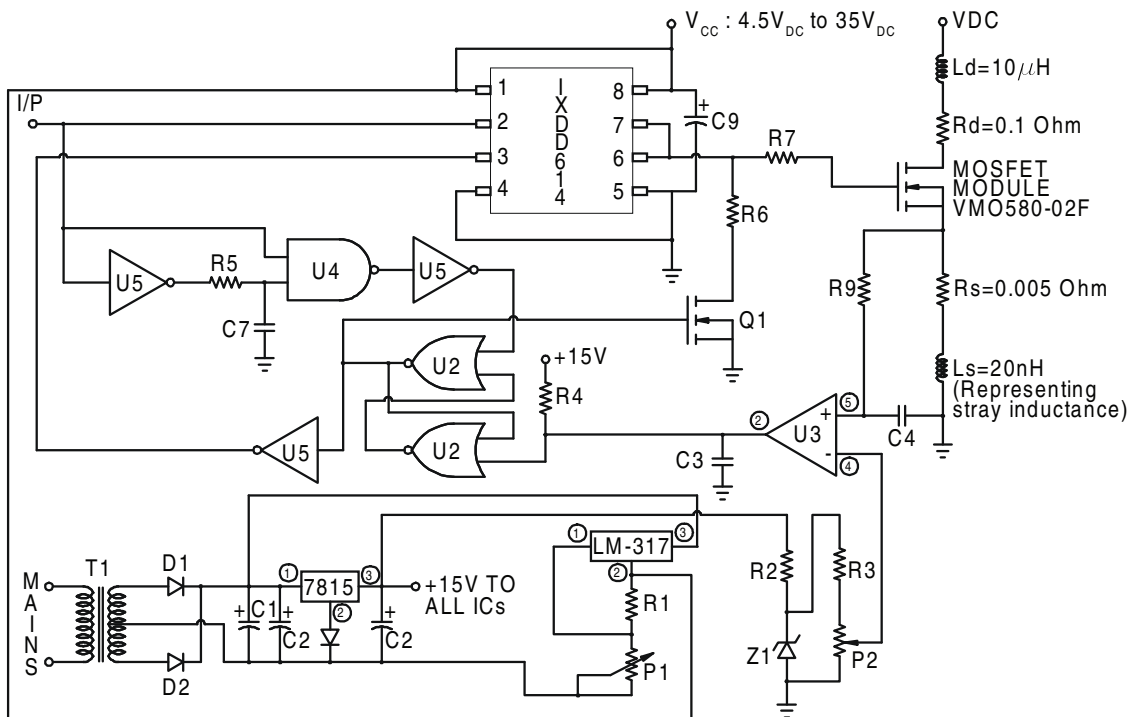


Figure 12 Soft turn-off Evaluation Circuit for IXDD609 and IXDD614



**Bill of Materials for Figure 12****Resistors:**

R1: 240  
R2: 560  
R3: 10K  
R4: 5K  
R5: 1Meg  
R6: 1K5  
R7: Rg-T.B.D.  
R8: 1Meg

**Capacitors:**

C1: 1000mF;35VWDC  
C2: 22mF, 63 VWDC  
C3: 1pF, silver dipped mica  
C4: 100pF silver dipped mica  
C5: 0.1mF, 35WDC Tantalum  
C6: 0.1mF, 35VWDC Tantalum  
C7: 1pF silver dipped mica  
C8: 0.1mF, 35VWDC Tantalum  
C9: 0.1mF, 35VWDC Tantalum  
C10: 0.1mF, 35VWDC Tantalum

**Diodes:**

D1: 1N4002 or BA 159  
D2: 1N4002 or BA 159

**Zener Diodes:**

1. Z1: 1N821

**Voltage Regulators:**

1. 7815  
2. LM317T

**Transistors:**

1. Q1: 2N7000

**ICs:**

U1: IXDD609SI or IXDD614SI  
U2: CD4001  
U3: LM339  
U4: CD4011  
U5: CD4049  
U6: IXDD609YI or IXDD614YI

Note: Use either U1 or U6 but not both.

**Trimmers:**

P1: 5K, 3006P Bourns or Spectrol  
P2: 1K, 3006P Bourns or Spectrol

Figure 13 +VE and -VE and Component Layout with Silk-Screen Diagram

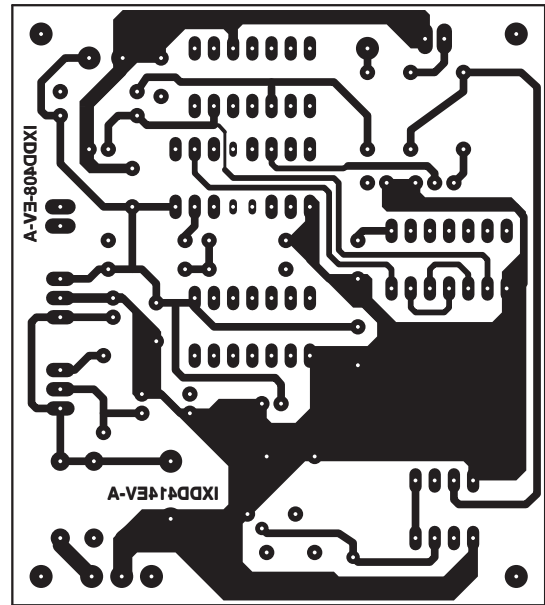
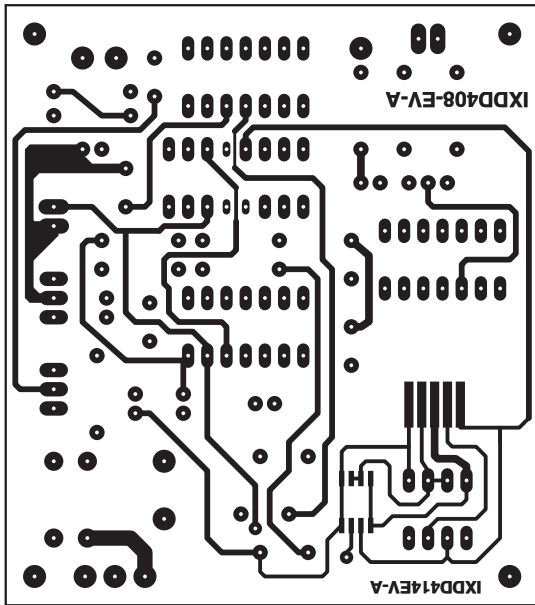
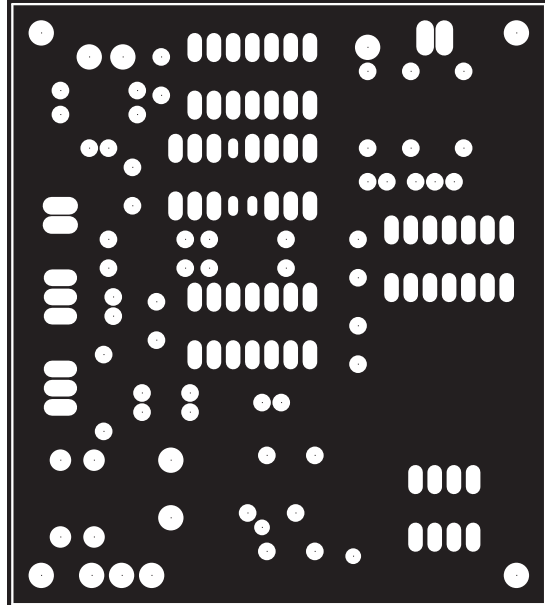
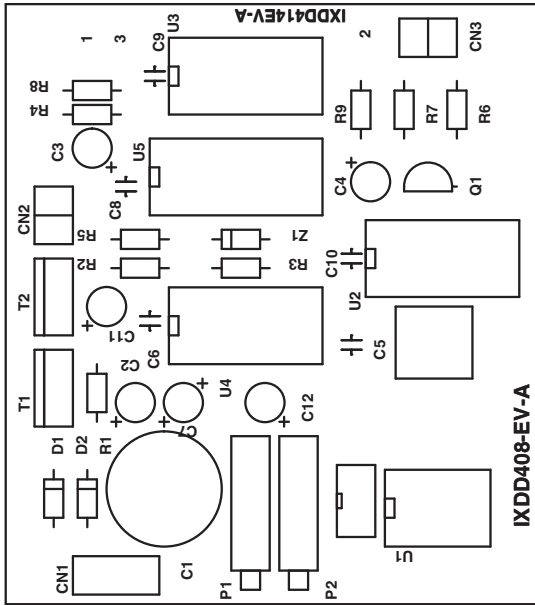


Figure 14 Basic Charge Pump Doubler

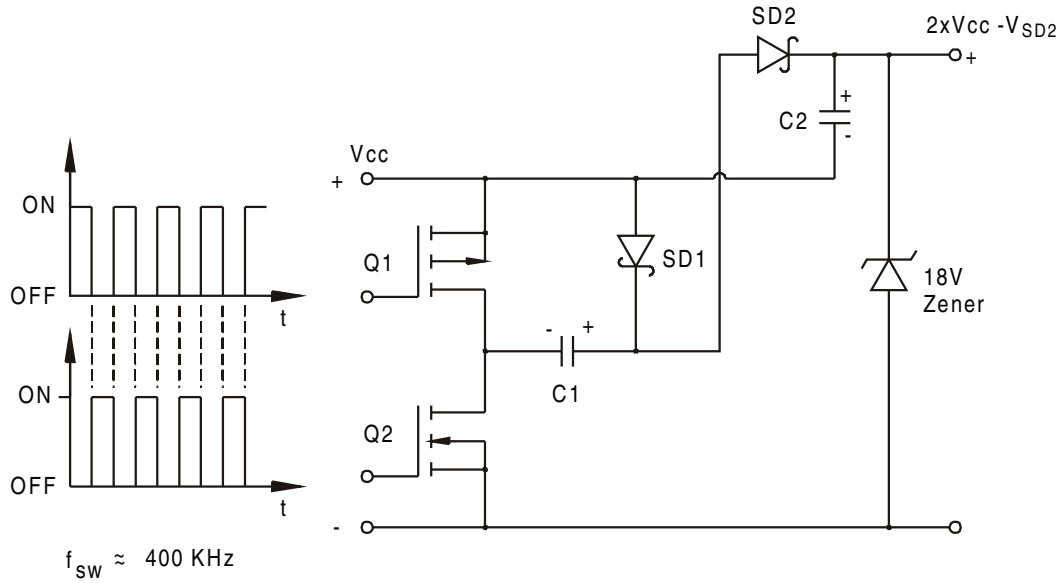
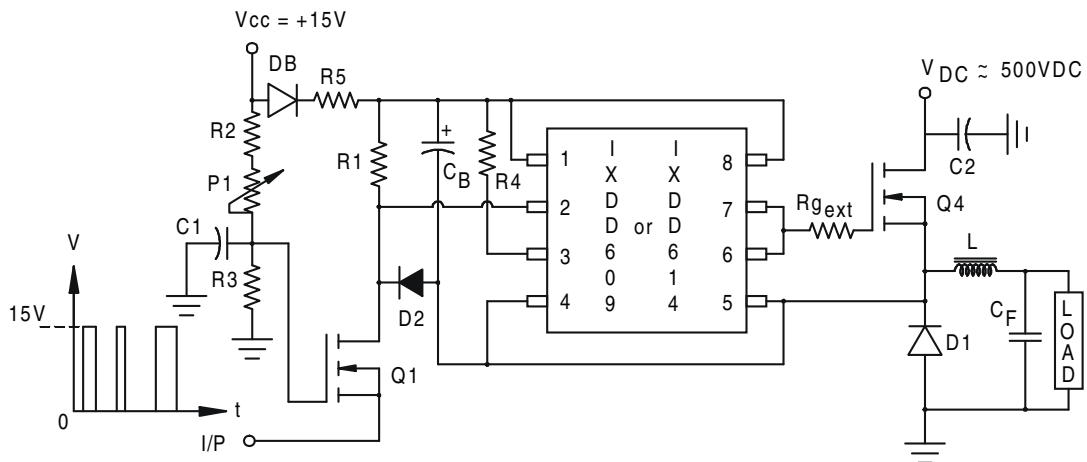


Figure 15 Basic Bootstrap Gate Drive Technique



Q1 : IXTU01N100  
DB : DSEP9-06CR  
D1 : DSEC60-12A  
D2 : 1N5817  
C1 : 20MFD,25V  
C2 : 20MFD,1000 Volts,CSI 10DC0020  
CB : 10MFD,25VDC  
P1 : 5K Trim pot

R<sub>g<sub>ext</sub></sub>: 1.0 Ohm to 4.7 Ohm  
CF : GE A28F5601  
0.1MFD,1000 Volts  
R1 : 1K  
R2 : 10K  
R3 : 2K  
R4 : 10K  
R5 : 1 Ohm  
L : 5μH,DALE IH-5

Figure 16 turn-off Enhancement Methods

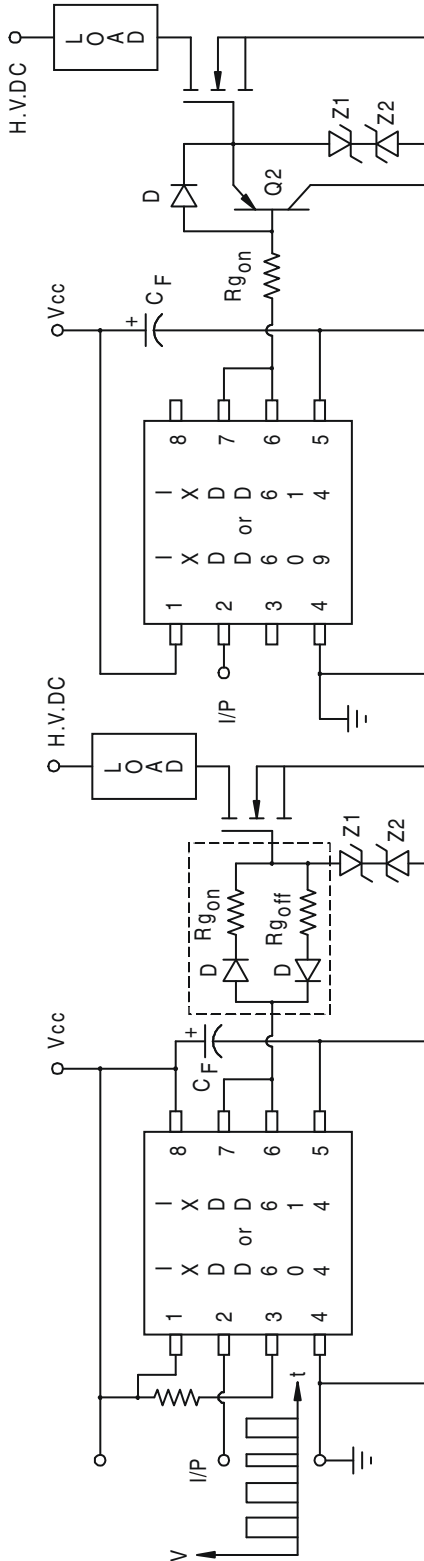


Figure 17 Technique To Boost Current Output and Provide -VE Bias To Achieve Faster turn-off For High Power MOSFET And IGBT Modules

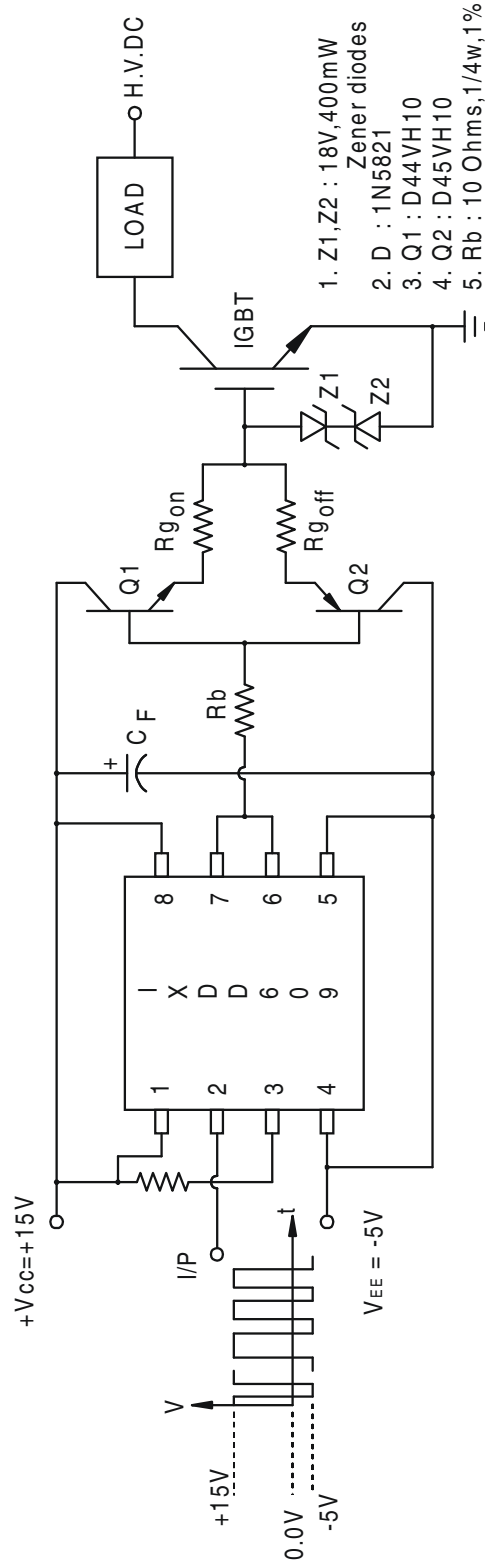
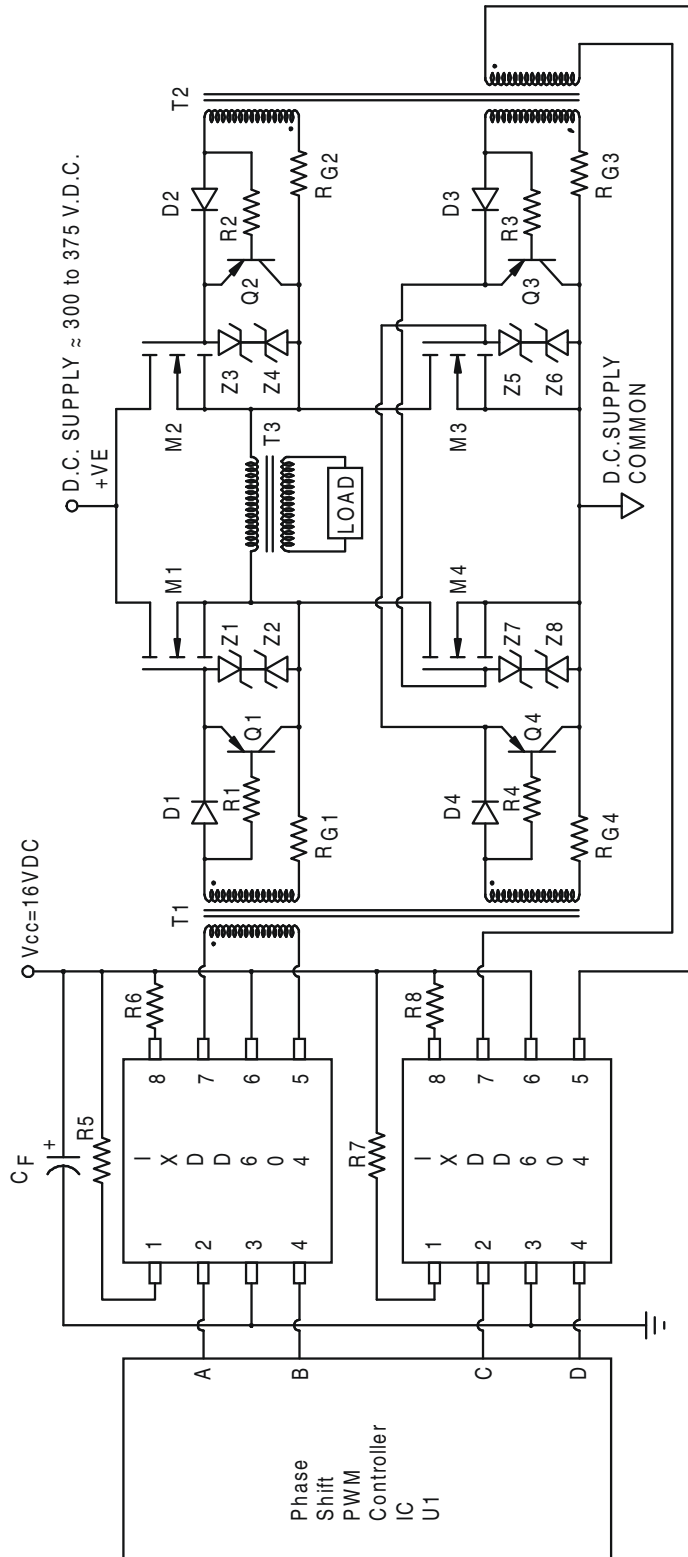


Figure 18 Transformer Coupled Gate Drive Arrangement For "H" Bridge In a Phase Shift PWM Controller at Fixed Switching Frequency



**SUGGESTED PARTS:**

1. U1 : T.I. UC3879
2. T1,T2 : Coilcraft Part No. SD250-3
3. Q1,Q2,Q3,Q4 : 2N2905A
4. D1,D2,D3,D4 : DSEP8-02A IXYS HiPerFRED
5. T3 : OUTPUT Transformer
6. CF : 22MFD,35 WVDC Tantalum Capacitor
7. R1,R2,R3,R4 : 560 Ohms, ¼ w,1% Metal film
8. M1,M2,M3,M4 : IXFN55N50 IXYS HiPerFET or IXFN80N50 IXYS HiPerFET
9. Z1,Z2,...Z8 : 18V, 400mW Zener diodes.
10. RG1,RG2,RG3,RG4 : 3.3 Ohms, ¼ w, 1% Metal Film resistors.
11. R5,R6,R7,R8 : 10K, ¼ w, 5%



Figure 19 3-Phase AC Motor Drive Schematic Showing How IXYS CBI (Converter-Brake-Inverter) Module Can Be Driven By IXDD614 Using Optocouplers - All Protection Features Are Incorporated

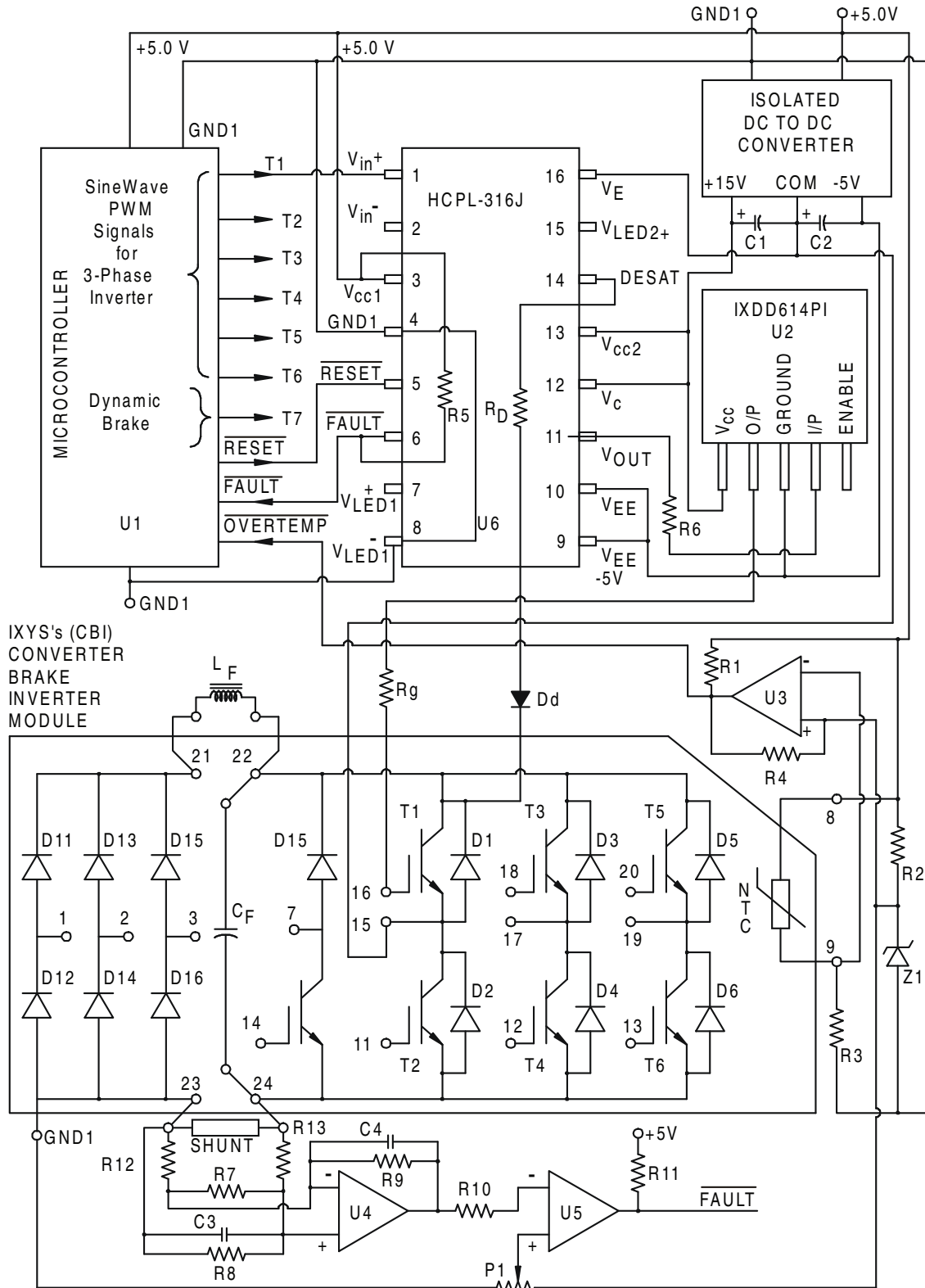
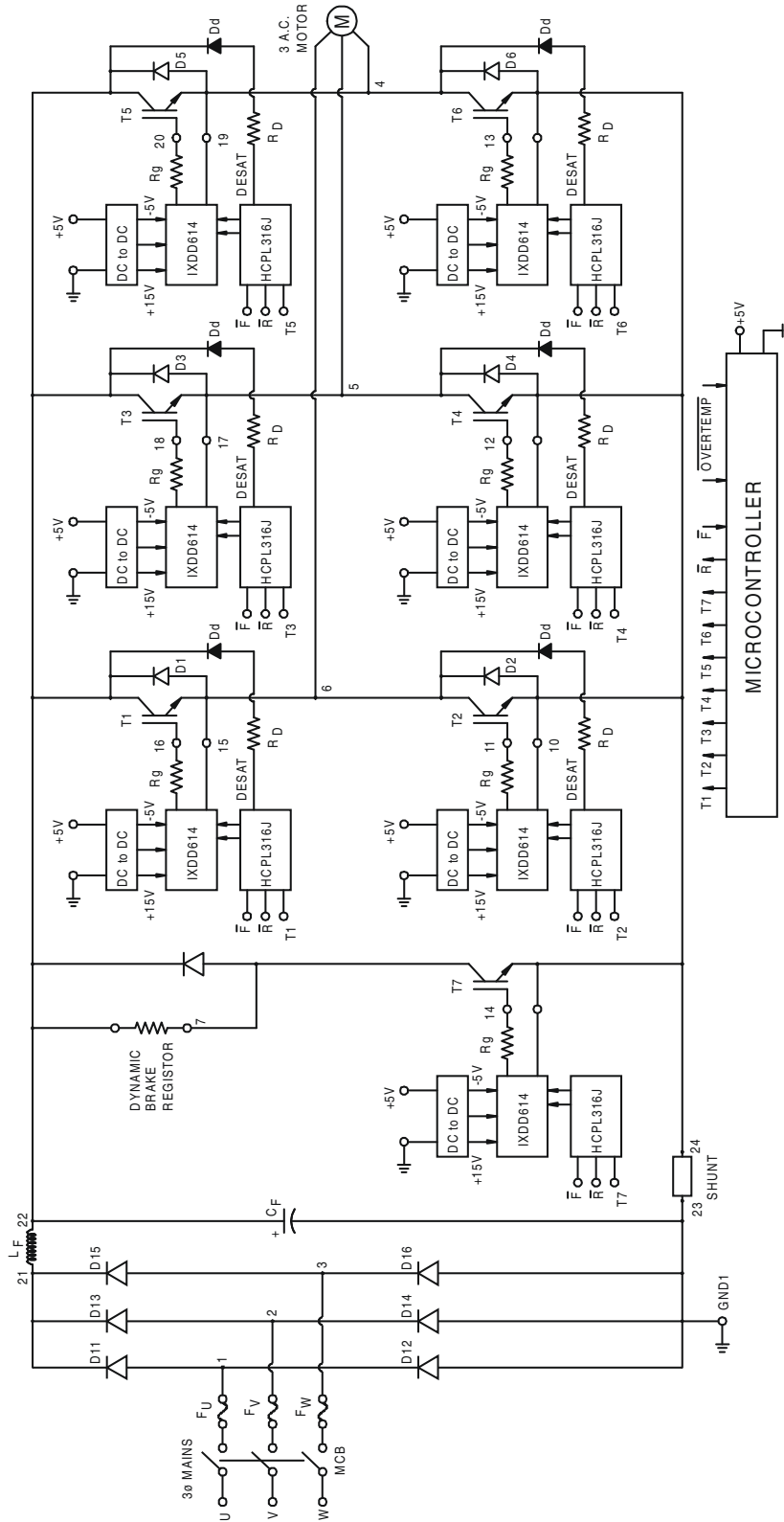


Figure 20 IXYS Converter, Brake Inverter (CBI) Module Being Driven By IXDD614 With Optocoupler and Desat, Overtemp, and Short Circuit/Overload Protections



- NOTES: 1. ALL  $\bar{F}$  = FAULT SIGNALS ARE TIED TOGETHER (BEING OPEN COLLECTOR) AND FED INTO MICROCOMPUTER.  
 2. ALL  $\bar{R}$  = RESET SIGNALS ARE TIED TOGETHER AND FED TO HCPL-316J.  
 3. OVERTEMP AND OVERLOAD/SHORT CIRCUIT FAULT SIGNALS ARE GENERATED AS PER FIG(16). OVERTEMP IS ALSO FED IN MICROCOMPUTER.

**Bill of Materials for Figure 19 and Figure 20****Resistors:**

R1: 10K, 1/4W, 1% MFR  
R2: 560 Ohms, 1/4W, 1% MFR  
R3: 10K, 1/4W, 1% MFR  
R4: 2.2 MegOhms, 1/4W, 5%  
R5: 10K, 1/4W, 1% MFR  
R6: 100 Ohms, 1/4 W, 1% MFR  
R7: 20K, 1/4W, 1% MFR  
R8: 61.9K, 1/4W, 1% MFR  
R9: 61.9K, 1/4W, 1% MFR  
R10: 10K, 1/4W, 1% MFR  
R11: 10K, 1/4W, 1% MFR  
R12: 1.24K, 1/4W, 1% MFR  
R13: 1.24K, 1/4W, 1% MFR  
Rg: T.B.D. based on  $T_{on}$ ,  $T_{off}$ , & size of IGBT  
RD:100 Ohms,1/4 w, 5%  
P1: 10K Trimpot, Bourns 3006P or Spectrol  
SHUNT : 75 mV @ full load current

**Capacitors:**

C3, C4: 33 pF, silver dipped mica  
CF: Electrolytic Filter Capacitor with very low ESR & ESL and screw type terminals to handle high ripple current. Voltage rating is based on DC Bus plus AC ripple Voltage

**Diodes:**

Dd: General Semiconductor make,  
RGP02-20E, 0.5A, 2000V, trr: 300ns

**Zener Diodes:**

Z1: Zener LM336, 2.5 Volt

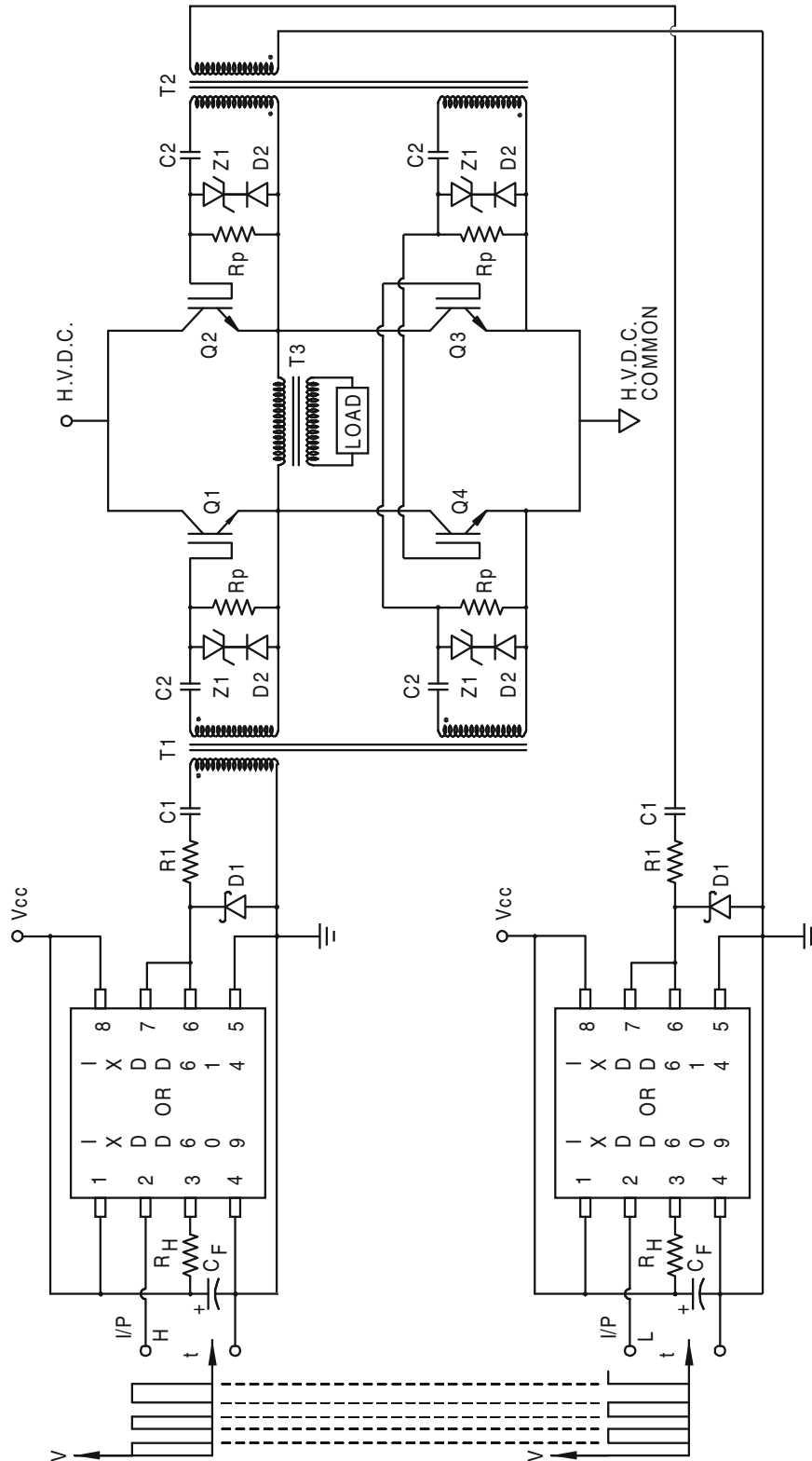
**Inductors:**

LF: Gapped DC Choke  
for filtering rectified power

**Semiconductors:**

U3: LM339 Comparator  
U4 : LM-101 Op Amp  
U5: LM339 Comparator  
CBI Module: IXYS Corporation Type Nos:  
MUBW 50-12A8 or any MUBW module  
from CBI 1, CBI 2 or CBI 3 series  
Microcontroller: T.I. TMS320F240  
with embedded software for AC Drive,  
using brake feature.  
IXDD614 Driver chip: 7 required to  
implement A.C.Drive, using Brake feature  
HCPL316J( Optocoupler) : 7 required to  
implement A.C.Drive With Brake feature.  
Isolated DC to DC Converter: 7 required  
with specified isolation.

Figure 21 IXYS Converter, Brake Inverter (CBI) Module Being Driven By IXDD614 With Optocoupler and Desat, Overtemp, and Short Circuit/Overload Protections



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